

# The Bipolar Theory of the Field-Effect Transistor: X. The Fundamental Physics and Theory (All Device Structures) \*

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**Abstract:** This paper describes the foundation underlying the device physics and theory of the semiconductor field effect transistor which is applicable to any devices with two carrier species in an electric field. The importance of the boundary conditions on the device current-voltage characteristics is discussed. An illustration is given of the transfer DCIV characteristics computed for two boundary conditions, one on electrical potential, giving much higher drift-limited parabolic current through the intrinsic transistor, and the other on the electrochemical potentials, giving much lower injection-over-the-barrier diffusion-limited current with ideal 60mV per decade exponential subthreshold roll-off, simulating electron and hole contacts. The two-MOS-gates on thin pure-body silicon field-effect transistor is used as examples

**Key words:** bipolar field-effect transistor theory; MOS field-effect transistor; electric potential; electrochemical potential; boundary conditions.

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## 1 Introduction

Electrical conduction in semiconductor devices contains two currents from two electrical charge carrier species, the electrons and the holes, which are quasi-particles in the one-particle representation of the energy band model of the many electrons and ions in a crystalline solid. Most devices are electrical and operate in externally applied electric fields. We will exclude the magnetic devices in this report. The theory of the electrical characteristics or terminal currents versus terminal voltages of semiconductor devices has been obtained by simultaneously solving six coupled differential equations known as the Shockley Equations<sup>[1,2]</sup>, usually given in the Cartesian coordinate,  $\mathbf{r} = (x, y, z)$ . The first of the six Shockley Equations is the Poisson Equation of the electromagnetic theory<sup>[3]</sup>, given in (1) below. It relates the divergence of the electric field,  $\mathbf{E}(\mathbf{r}, t)$  [which is derivable by the gradient of a scalar potential (Magnetic field is not included.),  $\mathbf{E}(\mathbf{r}, t) = -\nabla v(\mathbf{r}, t)$ , known as the electric potential  $v(\mathbf{r}, t)$ ] to the net space-charge density from the mobile electrons and holes,  $qn(\mathbf{r}, t)$  and  $qp(\mathbf{r}, t)$ , and the fixed and variable trapped charges,

$qP_{IM}(\mathbf{r}) - qn_T(\mathbf{r}, t)$ , in the volume and on the surface of the physical structure of the device or in the interface layer between the device and its surrounding. The current continuity equations, given by (2), (3), and (4) below, relate the divergence of the densities of the electron, hole and trapped electron currents,  $\mathbf{j}_N(\mathbf{r}, t)$ ,  $\mathbf{j}_P(\mathbf{r}, t)$  and  $\mathbf{j}_T(\mathbf{r}, t)$  flowing in the physical structure and through the surface and interface of the device. Included are the net generation, or generation less recombination, of electrons =  $g_N(\mathbf{r}, t) - r_N(\mathbf{r}, t)$ , holes =  $g_P(\mathbf{r}, t) - r_P(\mathbf{r}, t)$ , and net electron trapping =  $r_N(\mathbf{r}, t) - g_N(\mathbf{r}, t) - r_P(\mathbf{r}, t) + g_P(\mathbf{r}, t)$ <sup>[1,2,5]</sup> which is frequently omitted.

$$+\nabla \cdot (\epsilon_S \mathbf{E}) = \rho(\mathbf{r}, t) = q(p - n - P_{IM} + n_T)$$

Poisson Equation (1)

$$+\nabla \cdot \mathbf{j}_N + q(g_N - r_N) = q\partial n / \partial t$$

Electron Current Continuity Equation (2)

$$-\nabla \cdot \mathbf{j}_P + q(g_P - r_P) = q\partial p / \partial t$$

Hole Current Continuity Equation (3)

$$+\nabla \cdot \mathbf{j}_T + q(g_P - r_P) - q(g_N - r_N) = q\partial n_T / \partial t$$

Electron Current Continuity Equation (4)

The remaining two are the electron and hole current equations, which show explicitly the origins of the electrical currents; the current due to drift of the charged particles from the electrical force arisen from

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the Coulomb Law and the current due to diffusion of the charged particles in the concentration gradient due to the statistics from random scattering of the many particles:

$$\mathbf{j}_N = +q\mu_n n \mathbf{E} + qD_n \nabla n$$

Electron Drift and Diffusion Currents (5)

$$= -q\mu_n n \nabla v_N$$

Electron Electrochemical Current (5A)

$$\mathbf{j}_P = +q\mu_p p \mathbf{E} - qD_p \nabla p$$

Hole Drift and Diffusion Currents (6)

$$= -q\mu_p p \nabla v_P$$

Hole Electrochemical Current (6A)

The drift and diffusion currents, (5) and (6), are represented in an alternative form shown in (5A) and (6A), which are the gradients of the electron and hole electrochemical potentials,  $v_N(\mathbf{r}, t)$  and  $v_P(\mathbf{r}, t)$ , or the electrochemical field for electrons and holes,  $\mathbf{E}_N = -\nabla v_N$  and  $\mathbf{E}_P = -\nabla v_P$ , and which are just the exponential representations or the Maxwellian-Boltzmann representations of the electron and hole concentrations, given by

$$n(\mathbf{r}, t) = n_i \exp\{q[v(\mathbf{r}, t) - v_N(\mathbf{r}, t)]/k_B T\} \quad (7)$$

$$p(\mathbf{r}, t) = n_i \exp\{q[v_P(\mathbf{r}, t) - v(\mathbf{r}, t)]/k_B T\} \quad (8)$$

These two electrochemical potentials, one for electrons and one for holes, were coined by Shockley in his 1949 classic, the 64-page invention paper of the bipolar junction transistors<sup>[4]</sup> as the quasi-Fermi potentials, which he doubly emphasized as the non-equilibrium quasi Fermi levels, since they approach the Fermi level (potential) defined at electrical equilibrium or zero currents<sup>[1]</sup>. The coefficients and constants here have the traditional meaning,  $q$  = electron charge,  $k_B$  = Boltzmann constant,  $(\mu_n, D_n, \mu_p, D_p)$  = electron and hole mobilities and diffusivities, which are related by the Einstein relationship at thermal equilibrium,  $D/\mu = k_B T/q$ ,  $T$  = electron and hole temperatures or lattice temperature at thermal equilibrium<sup>[1]</sup>. At high electric fields, the near-equilibrium Boltzmann representation (or energy distribution) of the electrons and holes is extended to the Maxwellian representation in which the  $T$  would be the hot electron temperature  $T_E$  and hot hole temperature  $T_H$  respectively in the two exponential Maxwellian distributions<sup>[1]</sup>.

There are actually a seventh electrical current equation and an eighth neutral particle flux equation<sup>[5]</sup>. The seventh is the continuity equation of the electrical current due to the mobile trapped charges or the mobile charged traps, by drift and diffusion, in the same form as the two continuity equations of the electrical currents due to the two mobile charges, electrons and holes. The eighth continuity equation of the neutral particle flux is due to the mobile neutral traps

(due to impurity atoms and lattice defects, such as vacancies) via diffusion from their concentration gradients. Often we assume the trapped charges or the charged traps are immobile, i. e. with zero mobility and diffusivity so  $\mathbf{j}_T(\mathbf{r}, t) = 0$  in (4)<sup>[5]</sup>. But, in a most important branch of diode-transistor device physics and engineering and circuit applications, the charged and neutral traps, which consist of foreign impurities and lattice defects, can move, although very slowly in years. But their movements change the composition of the device which alters the electrical characteristics. These two continuity equations, the seventh and eighth, quantify the lifetimes (operating life and shelf life) of the device and the integrated circuits composed of many devices.

## 2 Boundary Conditions Determine the Currents

For a given device, such as the two-terminal diodes (p/n, metal/semiconductor or m/s, and metal/oxide/semiconductor or m/o/s or MOS), and the three- or four-terminal transistors, the electrical characteristics (such as currents flowing into the device terminals as a function of the voltages applied to the terminals) are completely determined by the values of three variables at the boundaries of the device. In the traditional representation of the model, these three variables are the electron and hole concentrations,  $n(\mathbf{r}, t)$  and  $p(\mathbf{r}, t)$  and the electric field  $\mathbf{E}(\mathbf{r}, t) = -\nabla v(\mathbf{r}, t)$  or the electric potential  $v(\mathbf{r}, t)$ . This is the preference of the chemists, because measurements of concentrations are routine to them. Electrical engineers are more familiar with potentials, in concept and in measurement capabilities. This electrical engineers' model, given by (5A) and (6A), using the two electrochemical potentials to represent the electron and hole concentrations, had been used extensively by Shockley when he introduced the quasi-Fermi potential concept in his 1949 invention of the p/n junction transistor<sup>[4]</sup>, and by the subsequent transistor engineers to design diode-transistor devices for integrated circuits and by students and teachers to learn transistor physics. These three electrical engineers' variables are the three potentials: the electric potential  $v(\mathbf{r}, t)$  and the electrochemical potentials for electrons and holes,  $v_N(\mathbf{r}, t)$  and  $v_P(\mathbf{r}, t)$ .

We shall now give some examples on how the boundary conditions or the boundary values of these three potentials can affect the D.C. steady-state current-voltage (DCIV) characteristics of the 2-MOS-Gate on thin pure-Base silicon field-effect transistor, known as the FinFET<sup>[2,12]</sup>.

To ease referencing, we list below the FinFET DCIV equations which were derived from the three equations of the six Shockley equations for the generation-recombination-trapping-free D. C. steady-state condition. Their derivations were given in the preceding article of this series, CJS11, which appeared in the last month issue<sup>[2]</sup>. The two-dimensional (2-D) terms from the longitudinal gradient of the longitudinal electric field (longitudinal electrical-field gradient or LEG) are excluded so this illustration is for long transistor with the channel physical length  $L$  much larger than the Debye length  $L_D$  since the LEG terms are scaled by  $(L_D/L)^2$  where  $L_D = [\epsilon_{Si} k_B T / q (n + p)]^{1/2}$ , first recognized and extensively illustrated by Shockley in 1949 as the crucial device parameter<sup>[4]</sup>, is about  $L_D \sim 25\mu\text{m}$  in pure silicon where  $n = p = n_i = 1.33 \times 10^{10} \text{ cm}^{-3}$  at  $T = 300\text{K}$ . So, for pure-silicon devices, the device is always small and multi-dimensional unless its dimensions are much larger than the pure Debye length of  $\sim 25\mu\text{m}$ . But for impure silicon, say  $p = P_{\text{IMPURITY}} = 10^{18} \text{ cm}^{-3}$  so  $n = n_i^2/p = (1.33)^2 \times 10^2$ ,

the Debye length is reduced to  $\sim 25\mu\text{m} \times (10^{10}/10^{18})^{1/2} \sim 2.5\text{nm}$ , making the 2D effects in state-of-the-art or next generation 25nm transistors not important, if built on heavily-impurity-doped silicon base-body. The effects on the DCIV characteristics from the neglected longitudinal electric field gradient, LEG, will be described in a later report in this series. The DCIV equations for the FinFET listed below are copied from [2], retaining the equation numbers of [2] but with the 2-D and impurity terms omitted. (For these omitted terms, please compare the following with the original Equations (57) to (70) in [2].) The coordinates are normalized:  $X = x/L_D$  from  $x = 0$  or  $X = 0$  to the thickness of the base-body silicon film,  $x = x_B$  or  $X = X_B$ ;  $Y = y/L$  from  $Y = 0$  to  $Y_0$  to 1, where  $Y_0$  is the internal flatband boundary which is the electrical boundary that divides the physical length of the base-body silicon film of length  $L$  or  $Y = y/L = L/L = 1$  into two electrical sections of electrical lengths  $Y_0$  and  $1 - Y_0$ .

$$(\partial U / \partial X)^2 = F^2(U, U_P, U_N, U_0) = + \exp(U - U_N) - \exp(U_0 - U_N) + \exp(U_P - U) - \exp(U_P - U_0) \quad (57)$$

$$U_{GS} - U_S = \text{sign}(U_S - U_0) \times (C_D / C_O) \times (\partial U / \partial X)_S \quad (\text{Valid for all } Y.) \quad (\text{The Voltage Equation.}) \quad (58)$$

$$\text{Integration of } U \text{ is from } U = U_0 \text{ to } U = U_S (x = x_B/2 \text{ to } x_B) \text{ and } Y, \text{ from } Y = 0 \text{ to } Y = 1. \quad (59)$$

$$X_B = 2 \int \text{sign}(U - U_0) \partial_X U / F \quad (\text{Valid for all } Y.) \quad (\text{The Thickness Equation}) \quad (60)$$

$$I_N = + q D_n n_i (W/L) L_D (\partial U_N / \partial Y) \exp(-U_N) \int [\exp(+U) \partial_X U / F(U, U_P, U_N, U_0)] \times 2 \quad (61)$$

$$= + q D_n n_i (W/L) L_D \int \partial_Y U_N \exp(-U_N) \int [\exp(+U) \partial_X U / F(U, U_P, U_N, U_0)] \times 2 \quad (62)$$

$$I_P = + q D_p n_i (W/L) L_D (\partial U_P / \partial Y) \exp(+U_P) \int [\exp(-U) \partial_X U / F(U, U_P, U_N, U_0)] \times 2 \quad (63)$$

$$= + q D_p n_i (W/L) L_D \int \partial_Y U_P \exp(+U_P) \int [\exp(-U) \partial_X U / F(U, U_P, U_N, U_0)] \times 2 \quad (64)$$

$$I_N = + q D_n n_i (W/L) [L_D / (Y)] \int \partial_Y U_N \exp(-U_N) \int [\exp(+U) \partial_X U / F(U, U_P, U_N, U_0)] \times 2 \quad (65)$$

$$I_P = + q D_p n_i (W/L) [L_D / (1 - Y)] \int \partial_Y U_P \exp(+U_P) \int [\exp(+U) \partial_X U / F(U, U_P, U_N, U_0)] \times 2 \quad (66)$$

$$(y_0/x_B) = (\partial U_{N_0} / \partial y) \cdot \exp(U_0 - U_{N_0}) / \int (\partial U_N / \partial y) \partial y \int [\exp(U - U_N) \partial X] \times 2 \quad (x = 0 \rightarrow x_B/2; y = 0 \rightarrow y_0) \quad (67)$$

$$(L - y_0)/x_B = (\partial U_{N_0} / \partial y) \cdot \exp(U_0 - U_{N_0}) / \int (\partial U_N / \partial y) \partial y \int [\exp(U - U_N) \partial X] \times 2 \quad (x = 0 \rightarrow x_B/2; y = y_0 \rightarrow L) \quad (68)$$

$$(L - y_0)/x_B = (\partial U_{P_0} / \partial y) \cdot \exp(U_{P_0} - U_0) / \int (\partial U_P / \partial y) \partial y \int [\exp(U_P - U) \partial X] \times 2 \quad (x = 0 \rightarrow x_B/2; y = y_0 \rightarrow L) \quad (69)$$

$$(y_0/x_B) = (\partial U_{P_0} / \partial y) \cdot \exp(U_{P_0} - U_0) / \int (\partial U_P / \partial y) \partial y \int [\exp(U_P - U) \partial X] \times 2 \quad (x = 0 \rightarrow x_B/2; y = 0 \rightarrow y_0) \quad (70)$$

There are three potential variables,  $U_N(Y)$ ,  $U_P(Y)$  and  $U(X, Y)$  with their two internal values at the two  $\text{SiO}_2/\text{Si}$  interfaces,  $x = 0$  and  $x = x_B$ , and at

the mid-base minimum or maximum, respectively given by  $U(X = 0, Y) = U(X = X_B, Y) = U_S(Y)$  and  $U(X = X_B/2, Y) = U_0(Y)$ . To obtain the electron

and hole channel currents from (61) to (64), we need to relate the three of the four potentials to the fourth, the  $Y$  integration potential. For example, to compute the electron surface and volume channel current,  $I_N$ , using the differential equation (61) with a single integration in  $X$  or  $\partial_X U$  for the electron charge,  $Q_N$ , or using the integral equation (62), which is the solution of the differential equation (61) with two integrations, in  $X$  or  $\partial_X U(X, Y)$  then in  $Y$  or  $\partial_Y U_N(Y)$ , we need to relate  $U_S(Y)$ ,  $U_0(Y)$  and  $U_P(Y)$  to  $U_N(Y)$ . We have two internal equations, the Voltage Equation given by (58) and the Thickness Equation given by (60). We need a third equation, to relate  $U_P(Y)$  to  $U_N(Y)$ . It has been arbitrarily set without a device physics basis in all previous work. For our newly discovered bipolar nature of all FETs, this third equation or relation to relate  $U_P$  to  $U_N$  in order to compute the electron channel current in the Bipolar FET, is obtained from the hole current equations, either (63) or (64), and the implicit coupling of the electrons with the holes is through the space-charge density of the Poisson Equation. So, this is a recursive iteration exercise by successive numerical approximation within each recursive iteration cycle and by repeating the cycle (so named recursive, if not in conflict with another usage) until a specified convergence is reached, for example, the electron and hole currents,  $I_N$  and  $I_P$ , no longer change more than a user specified percentage from the previous recursive iteration cycle to the present recursive iteration cycle. The obvious starting point is the unipolar solution, that is, for  $I_N$  let  $P = 0$ , and for  $I_P$  let  $N = 0$ , because there is enough equations, i. e., the Voltage and Thickness Equations, (58) and (60), for the three variables, the electric and electron-electrochemical potentials,  $U_S(Y)$ ,  $U_0(Y)$ , and  $U_N(Y)$ , at any  $Y$  in the internal channel and at its two boundaries at  $Y = 0$  and  $Y = 1$ . For convenience and on account of device physics, we have called it in our CJS05 report<sup>[11]</sup> the 0<sup>th</sup> cycle or the initial guesses or guess of the recursive iteration algorithms. However, these initial solutions based on  $N = 0$  or  $P = 0$ , correctly called the Unipolar solutions, are not strictly the correct initial solutions of the problem formulated in the three potentials, but rather they are those for the Drift and Diffusion formulation. The senior author also recognized the two obvious algorithms or routes to carry out the recursive iteration solution and we coined them the cross-linked double-string algorithm and the zig-zag single-string algorithm<sup>[11]</sup>. The final and converged numerical DCIV characteristics from the two algorithms should be identical if the stop criterion is set to a high degree of accuracy.

In addition, the internal boundary of the two-section model, first defined by the first author, in his 1991 – 1993 textbook to teach junior students in the device core course,  $0 \leq Y_0 \leq 1$ , can be computed from the four equations, (67) to (70), all should give the same numerical result when the user-defined convergence is reached and if the convergence criterion is set at a sufficiently high accuracy. This internal boundary, defined by  $Y_0$ , is necessary to compute the DCIV characteristics in the current saturate range when the field-effect transistor is electrically divided into two sections with electrical lengths of  $y_0$  and  $L - y_0$ , where  $y_0$  or  $Y_0 = y_0/L$  is the flatband boundary inside the transistor, which are called by us<sup>[11]</sup> as the emitter section and collector section, just like those in the Bipolar Junction Transistor coined by Shockley in 1949<sup>[4]</sup>. This electrical division is also important to compute the presently omitted 2-D LEG effects on the DCIV characteristics, which was not recognized by device modeling engineers, although the two section model was a prominent feature introduced and exhaustively described, based on device physics, by Shockley in his 1952 invention article on the Junction-Gate Field-Effect Transistor (JGFET) which has two identical n/p junction gates and a p-type volume channel<sup>[6]</sup> and which was analyzed with high-power exotic analytical mathematics by Prim and Shockley in 1953 as an introductory exercise by the young Prim to learn the analytical mathematical solution of transistors<sup>[7]</sup> in the pre-desktop computer era, without the canned numerical computer programs as device simulators of today, which has replaced the physics-based analytical solutions, removing the incentive of the education to recent students, teachers and practicing engineers on understanding fundamental diode-transistor device physics.

The DCIV curves are highly dependent on the  $Y$  boundary conditions set by the user for the four variables  $U_S(Y)$ ,  $U_0(Y)$ ,  $U_N(Y)$  and  $U_P(Y)$  at the two ends of the transistor's thin base,  $Y = 0$  at the source and  $Y = 1$  at the drain. Two cases are described below to illustrate.

The least restrictive case is the boundary condition of  $U_0(Y = 0) = U_{SB} = 0$  and  $U_0(Y = 1) = U_{DB} \geq 0$  with  $U_{GB} \geq 0$  for the electron channel current,  $I_N$ , and the corresponding bias configuration or boundary condition of  $U_0(Y = 0) = U_{SD} \leq 0$  and  $U_0(Y = 1) = U_{DB} = 0$ , with  $U_{GD} \leq 0$  for the hole channel current,  $I_P$ . In this case, source and drain electric potential boundary contacts are the two end points located at the mid-plane of the thin silicon base-body, the source point at  $(x = x_B/2, y = 0)$  and the drain point at  $(x = x_B/2, y = L)$  of the "intrinsic" transistor. "Intrinsic"

means the geometry definition of the ideal transistor structure, excluding the fringe fields at the corners. They are exactly the boundary points assumed in solving the  $y$ -independent Poisson equation so there is no physical reality conflict. Since  $U_N(Y)$  and  $U_P(Y)$  are not specified in the base-body volume and at the boundaries,  $Y = 0$  and  $Y = 1$ , the electron and hole currents,  $I_N$  and  $I_P$ , and the magnitude and spatial variations of their concentrations,  $P$  and  $N$ , are not restricted and are set only by the voltage applied to the two boundary points, labeled Source and Drain. Since the boundary conditions are imposed on the electric potential,  $U(x, y)$ , that controls the drift current, and not the electrochemical potentials of electrons and holes, that controls the diffusion currents, the channel currents are mobile carrier concentration limited drift currents, and the concentration gradient limited diffusion currents are negligible. So, the electron and hole currents would be higher than those from another set of boundary conditions imposed on  $U_N(Y)$  and  $U_P(Y)$ , that would bring out the diffusion limitation, such as those computed by us for the bipolar theory of the MOS field effect transistor using the electrochemical potential approach<sup>[8,9]</sup> with the boundary conditions of  $U_N(Y = 0) = U_{SB} = 0$  and  $U_N(Y = 1) = U_{DS} \geq 0$ , and gate voltage of  $U_{GB} \geq 0$  for the electron channel current  $I_N$ ; and  $U_P(Y = 0) = U_{SB} \leq 0$  and  $U_P(Y = 1) = U_{DB} = 0$ , and gate voltage of  $U_{GB} \leq 0$  for the hole channel current  $I_P$ . These boundary conditions on  $U_N(Y)$  and  $U_P(Y)$  at  $Y = 0$  and  $Y = 1$ , correspond to electron and hole contacts, which would then limit the electron and hole currents and also the spatial variations of the electron and hole concentrations by the current-voltage characteristics of the contacts, whose physical structures, such as the  $p^+/i$ ,  $n^+/i$  and  $m/i$  diodes, are excluded from the intrinsic transistor. Even more restricted conditions on  $U_N(Y)$  and  $U_P(Y)$  have been imposed by others<sup>[10]</sup>, not just at the boundaries, but also in the interior or the base-body, which are out of reach and physically unrealizable.

Numerical illustration to compare the transfer DCIV,  $I_N$  and  $I_P$  versus  $V_{GS}$ , at  $V_{DS} = +0.5V$  is given in Fig. 1, for the two different boundary conditions: (BC-1)  $BC - U_0$  of  $U_0(Y = 0) = U_{SB} = 0$  and  $U_0(Y = 1) = U_{DB} \geq 0$ ,  $U_N(Y)$  and  $U_P(Y)$  are not restricted; and (BC-2) consisting of  $BC - U_N$  of  $U_N(Y = 0) = 0$  and  $U_N(Y = 1) = U_{DB} \geq 0$  with  $U_{GB} \geq 0$ , and  $BC - U_P$  of  $U_P(Y = 0) = U_{SB} \leq 0$  and  $U_P(Y = 1) = U_{DB} = 0$  with  $U_{GD}$  and  $U_{GB} \leq 0$ . The (BC-2) curves show the contact controlled DCIV characteristics with lower surface channel currents in both the large drift-dominated “inversion” current range and the small diffusion-

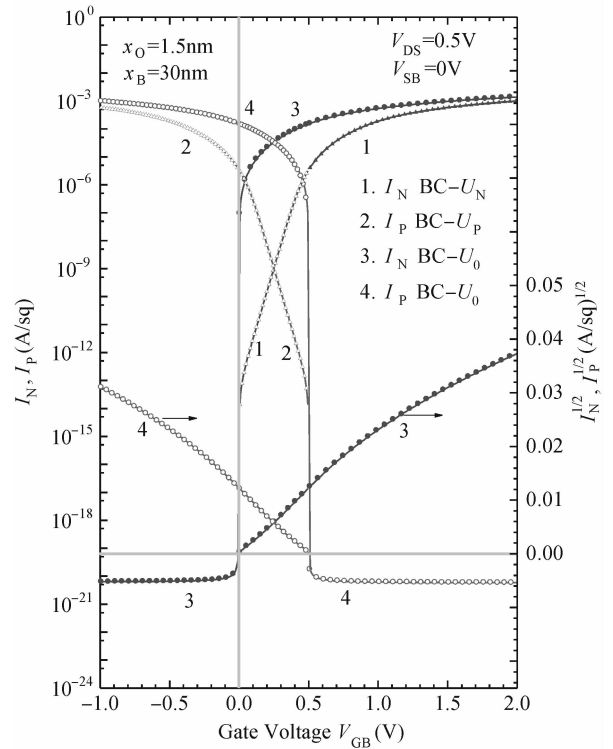


Fig. 1 Transfer DCIV characteristics for the two different boundary conditions shown in the figure.

dominated subthreshold range of the classical 60mV per decade decrease, which is limited by the electron contact  $n^+/i$  for  $I_N$  and hole contact  $p^+/i$  for  $I_P$  when the  $U_N$  and  $U_P$  values at the boundaries are specified by the user. The (BC-1) curves show much higher currents since the electrons and holes are not limited by boundary or contact conditions, resulting in the dominance of the space-charge-limited drift current that is power-law (parabolic) dependence on the gate voltage. The very abrupt cutoff, is an artifact from graphing on the semi-log scale of an ohmic or linear, or a power-law (parabolic) single-carrier mobile space-charge-limited  $I-V$  characteristics. The DCIV characteristics covering extended range of parameters are reported in the following article<sup>[11]</sup>.

### 3 Summary

The fundamental basis of the bipolar solutions of the bipolar MOS field effect transistor is reviewed to help show the importance of boundary conditions of the electric and electrochemical potentials on the DCIV characteristics of the transistor. The electron and hole surface channel currents are not limited by diffusion from concentration gradient, only drift from electric field when the boundary conditions are applied only to the electric potential. When the boundary values are imposed on the electrochemical potentials, the currents are limited by the assumed electron

or hole contact types to the source and drain, such as the diffusion-limited over-the-barrier injection-current from the  $n^+/i$  and  $p^+/i$  contacts, simulated by imposing the boundary values on  $U_N(Y)$  and  $U_P(Y)$  at the source  $Y = 0$  and drain  $Y = 1$  contacts, giving rise to the 60mV per decade current roll-off from the classical 1949-Shockley p/n junction diode  $\exp(U_{PN})$ .

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## References

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# 场引晶体管双极理论: X. 基本物理和理论(所有器件结构)<sup>\*,\*\*</sup>

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**摘要:** 本文描述半导体场引晶体管器件物理和理论所用的根本原则, 它适用电场中有两种载流子的器件. 讨论边界条件对器件电流电压特性的重要性. 作为例子, 计算两种边界条件下的转移直流电压特性: 电势边界给出很高、流进内禀晶体管、飘移限制抛物型电流, 电势边界仿真电子和空穴接触, 给出很低、越过势垒注入、扩散限制电流, 具有理想、每量级 60mV、指数型亚阈值区倾斜. 双 MOS 栅 薄纯基硅场引晶体管为典型结构.

**关键词:** 双极场引晶体管理论; MOS 场引晶体管; 电势; 电势; 电势; 边界条件

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