

双离子注入短沟道 MOS FET 的阈值 电压解析模型*

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本文对短沟道 MOSFET 沟道区的硼、砷离子注入分布采用二次函数及指数函数的分段函数分布近似，并利用格林函数法求解二维泊松方程，从而导出非均匀分布短沟道 MOS FET 的表面势和阈值电压的解析模型。它计及注入能量、剂量、退火温度、退火时间等工艺参数的影响，也包含了漏极电压 V_D 和栅氧化层厚度等因素的影响。本解析模型的结果与用 MINIMOS 数值模拟的结果符合得很好，具有简单、实用的特点。适用于改进有关电路分析程序例如 SPICE 中的模型。

主题词： 泊松方程，离子注入，解析解，表面势，边界条件

一、引言

随着集成电路规模的增大以及器件尺寸的缩小，MOS 场效应管的短沟道效应愈来愈受到人们的重视。通常可采用解析和数值模拟两种方法进行讨论。由于解析法具有简单、实用的优点，近年来有关研究工作日益增多。一些作者采用了沟道区杂质均匀分布的假设^[1-3]，所得模型不适合于沟道区杂质非均匀分布情况。尤其是在沟道长度较短时，非均匀掺杂引起沟道中电场分布不均匀的影响不可忽视。有的模型虽然考虑了非均匀掺杂分布，但在分析中采用了阶梯函数近似或动态平均模型^[1,4]，其实质仍然是均匀分布的模型。它们不能定量给出工艺参数对模型的影响。还有一些模型采用了非均匀分布，但包含了大量的余误差函数计算，较为复杂、费时^[5,6]。J.D. Kendall 等人的模型^[7]之局限在于仅仅考虑了掺杂分布的峰值在表面的情况，他们也未给出工艺参数与模型的定量关系。

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二、非均匀掺杂沟道的近似模型

对于较短沟道的 MOS 场效应管，沟道区往往由二次离子注入形成。通常注入方向的分布由高斯函数来描写：

$$N(y) = \frac{\phi}{\sqrt{2\pi}\Delta R_{p_0}} \exp \left[-\left(\frac{y - R_{p_0}}{\sqrt{2}\Delta R_{p_0}} \right)^2 \right] \quad (1)$$

其中 ϕ 为注入剂量； R_{p_0} 及 ΔR_{p_0} 分别为投影射程和投影标准偏差。它们可由 K. A. Picker^[1] 文中的有关数据拟合而得。若考虑离子注入的退火过程，则 R_p 及 ΔR_p 分别为：

$$R_p = R_{p_0} \quad (2-a)$$

$$\Delta R_p = \sqrt{2(\Delta R_{p_0}^2 + 2 \sum_i D_i t_i)} \quad (2-b)$$

D_i 和 t_i 分别是第 i 次退火处理的扩散系数和扩散时间。为便于计算并保持一定的精确度，可将(1)式近似为：

$$N(y) = \begin{cases} N_m \left[1 - \left(\frac{y - R_p}{\Delta R_p} \right)^2 \right] & (0 < y < R_p + 0.5\Delta R_p) \\ N_m \exp \left[-\frac{1.5}{\Delta R_p} (y - R_p - 0.5\Delta R_p) - 0.25 \right] & (y > R_p + 0.5\Delta R_p) \end{cases} \quad (3)$$

式中 $N_m = \frac{\phi}{\sqrt{2\pi}\Delta R_p}$ 。可以证明在 $R_p - 0.5\Delta R_p \leq y \leq R_p + 0.5\Delta R_p$ 内采用二次函数分布近似引进的误差小于 4%；在 $R_p + 0.5\Delta R_p \leq y \leq R_p$ 内采用指数函数分布的近似小于 6%。为清楚起见，(3)式可表示为：

$$N(y) = \begin{cases} N_{m1} \cdot (s_2 y^2 + s_1 y + s_0) & (\text{砷}) \\ N_{m1} \cdot \exp(s_1 y + s_0) & (\text{硼}) \end{cases} \quad (4)$$

$$N(y) = \begin{cases} N_{m2} (b_2 y^2 + b_1 y + b_0) & (\text{砷}) \\ N_{m2} \cdot \exp(b_1 y + b_0) & (\text{硼}) \end{cases} \quad (5)$$

其中

$$s_0 = 1 - \left(\frac{R_{pA1}}{\Delta R_{pA1}} \right)^2, \quad s_1 = \frac{2R_{pA1}}{(\Delta R_{pA1})^2}, \quad s_2 = -\frac{1}{(\Delta R_{pA1})^2},$$

$$s_3 = \frac{1.5R_{pA1}}{\Delta R_{pA1}} + 0.5, \quad s_4 = -\frac{1.5}{\Delta R_{pA1}}, \quad b_0 = 1 - \left(\frac{R_{pb}}{\Delta R_{pb}} \right)^2$$

$$b_1 = \frac{2R_{pb}}{(\Delta R_{pb})^2}, \quad b_2 = -\frac{1}{(\Delta R_{pb})^2}, \quad b_3 = \frac{1.5R_{pb}}{\Delta R_{pb}} + 0.5,$$

$$b_4 = -\frac{1.5}{\Delta R_{pb}}; \quad N_{m1} = \frac{\phi_{A1}}{\sqrt{2\pi}\Delta R_{pA1}}, \quad N_{m2} = \frac{\phi_b}{\sqrt{2\pi}\Delta R_{pb}}.$$

三、泊松方程的解

(1) 长沟道情况

假设杂质沿沟道方向的分布是均匀的。如图 1 所示，由耗尽层近似，泊松方程可写

为：

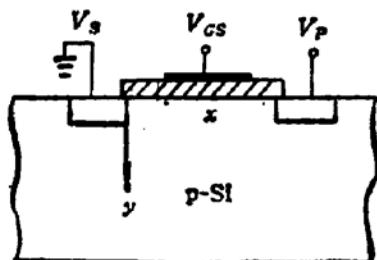


图 1 MOS 场效应管结构剖面图

$$\frac{d^2\phi(x \cdot y)}{dy^2} = \frac{qN(y)}{\epsilon_0\epsilon_{Si}} \quad (6)$$

对于砷和硼二次离子注入情况，

$$N(y) = N_{m1} e^{-\frac{1}{2}(\frac{y-R_{pA1}}{\Delta R_{pA1}})^2} - N_{m2} e^{-\frac{1}{2}(\frac{y-R_{pb}}{\Delta R_{pb}})^2} - N_0 \quad (7)$$

垂直于表面的电场 E_z 为：

$$E_z = - \left[\int_0^{y_d} - \frac{d^2\phi}{dy^2} \cdot dy \right] = \frac{q}{\epsilon_0\epsilon_{Si}} \int_0^{y_d} N(y) dy \quad (8)$$

式中 y_d 为沟道耗尽层厚度。长沟道 MOS 管的阈值电压为：

$$V_{TO} = V_{FB} + 2\phi_F + \frac{\epsilon_0\epsilon_{Si}}{C_{ox}} E_z = V_{FB} + 2\phi_F + \frac{qE_{ox}}{\epsilon_0\epsilon_{ox}} \int_0^{y_d} N(y) dy. \quad (9)$$

上式中 V_{FB} 为平带电压， ϕ_F 为费密势， t_{ox} 为栅氧化层厚度。利用上节引进的近似式，并假定 $R_{pb} > R_{pA1}$, $\Delta R_{pb} > \Delta R_{pA1}$, 而且 $R_{pA1} < y_d < R_{pb}$ 。其中 $R_{pA1} = R_{pA0} + 0.5\Delta R_{pA0}$, $R_{pb} = R_{p0} + 0.5\Delta R_{p0}$, 则(7)式可写为：

$$N(y) = \begin{cases} N_{m1}(s_1 y^2 + s_1 y + s_0) - N_{m2}(b_2 y^2 + b_1 y + b_0) - N_0 & (0 < y < R_{pA1}) \\ N_{m1} e^{(s_1 y^2 + s_1 y)} - N_{m2} (b_2 y^2 + b_1 y + b_0) - N_0 & (R_{pA1} < y < y_d) \end{cases} \quad (10)$$

于是便可得长沟道 MOS 管的阈值电压公式为：

$$V_{TO} = V_{FB} + 2\phi_F + \frac{qE_{ox}}{\epsilon_0\epsilon_{Si}} (I_A + I_B) \quad (11)$$

其中

$$\begin{aligned} I_A &= \frac{1}{3} (N_{m1} s_1 - N_{m2} b_2) R_{pA1}^3, \\ &+ \frac{1}{2} (N_{m1} s_1 - N_{m2} b_1) R_{pA1}^2 + (N_{m1} s_0 - N_{m2} b_0 - N_0) R_{pA1} \end{aligned} \quad (12)$$

$$\begin{aligned} I_B &= \frac{N_{m1} e^{s_1 y_d}}{S_4} (e^{s_1 y_d} - e^{s_1 R_{pA1}}) - \frac{N_{m2} b_2}{3} (y_d^3 - R_{pA1}^3) \\ &- \frac{N_{m2} b_1}{2} (y_d^2 - R_{pA1}^2) - (N_{m2} b_0 + N_0) \cdot (y_d - R_{pA1}) \end{aligned} \quad (13)$$

由(11)式显而易见阈值电压与离子注入的能量及剂量有关。 V_{TO} 可由改变注入条件来调节。

(2) 短沟道情况

对于短沟道 MOS 场效应管必须求解下述二维泊松方程:

$$\frac{\partial^2 \phi(x, y)}{\partial x^2} + \frac{\partial^2 \phi(x, y)}{\partial y^2} = \frac{qN(y)}{\epsilon_0 \epsilon_{Si}} \quad (14)$$

采用文献[9]中我们曾用过的方法,可以得到方程(14)的解为:

$$\begin{aligned} \phi_A(x, y) = V_n x + \frac{V_D}{l} \cdot x + \sqrt{\frac{2}{l}} \sum_n (C_n e^{r_n y} + D_n e^{-r_n y} + g_n y^2 + h_n y + i_n) \\ \cdot \sin r_n x \quad (0 < y < R_{pA}) \end{aligned} \quad (15)$$

$$\begin{aligned} \phi_B(x, y) = V_n + \frac{V_D}{l} x + \sqrt{\frac{2}{l}} \sum_n (\tilde{C}_n e^{r_n y} + \tilde{D}_n e^{-r_n y} + p_n e^{r_n} + q_n y^2 \\ + u_n y + v_n) \cdot \sin r_n x \quad (R_{pA} < y < y_d) \end{aligned} \quad (16)$$

式中 V_n 为内建势, V_D 为漏极电压, 其他参数为:

$$r_n = \frac{n\pi}{l},$$

$$f_n = \sqrt{\frac{2}{l}} \frac{q}{\epsilon_0 \epsilon_{Si}} \left(\frac{l}{n\pi} \right) [1 - (-1)^n],$$

$$g_n = -\frac{f_n}{r_n^2} (N_{mS} s_2 - N_{mb} b_2),$$

$$h_n = -\frac{f_n}{r_n^2} (N_{mS} s_1 - N_{mb} b_1),$$

$$i_n = -\frac{f_n}{r_n^2} (N_{mS} s_0 - N_{mb} b_0 - N_0) - \frac{2f_n}{r_n^4} (N_{mS} s_1 - N_{mb} b_1),$$

$$p_n = \frac{f_n N_{mb} e^{r_n}}{r_n^2 - r_n^4},$$

$$q_n = \frac{f_n N_{mb} b_2}{r_n^2},$$

$$u_n = \frac{f_n N_{mb} b_1}{r_n^2},$$

$$V_n = \frac{f_n (N_{mb} b_0 + N_0)}{r_n^2} + \frac{2f_n N_{mb} b_1}{r_n^4}$$

(15)与(16)式的推导可参阅本文附录。为了求得该两式中的待定系数, 假定电势 $\phi(x, y)$ 满足下述边界条件:

$$\phi_A(x, R_{pA}) = \phi_B(x, R_{pA}) \quad (17)$$

$$\left\{ \frac{\partial \phi_A(x, y)}{\partial y} \Big|_{y=R_{pA}} = \frac{\partial \phi_B(x, y)}{\partial y} \Big|_{y=R_{pA}} \right. \quad (18)$$

$$\left. \frac{\partial \phi_B(x, y)}{\partial y} \Big|_{y=y_d} = 0 \right. \quad (19)$$

$$\phi_A(x, 0) = V_G - V_{BS} + \frac{z_{oA} \epsilon_{Si}}{\epsilon_{ss}} \frac{\partial \phi_A}{\partial y} \Big|_{y=0} \quad (20)$$

通过计算可以得到 $C_n, D_n, \tilde{C}_n, \tilde{D}_n$ 分别为:

$$C_s = \frac{x_{35} + x_{34} - \frac{r_s x_{15} - x_{25}}{2 r_s x_{12}} - \frac{x_{34} x_{45}}{x_{42}} + x_{33} - \frac{r_s x_{15} + x_{25}}{2 r_s x_{11}}}{x_{33} - \frac{x_{34} x_{41}}{x_{42}}} \quad (21)$$

$$D_s = \frac{x_{45} - x_{41} C_s}{x_{42}} \quad (22)$$

$$\tilde{C}_s = C_s - \frac{r_s x_{15} + x_{25}}{2 r_s x_{11}} \quad (23)$$

$$\tilde{D}_s = D_s - \frac{r_s x_{15} - x_{25}}{2 r_s x_{12}} \quad (24)$$

其中 $x_{11} = e^{r_s R_p A_1}$, $x_{12} = e^{-r_s R_p A_1}$, $x_{13} = -x_{11}$, $x_{14} = -x_{12}$,
 $x_{15} = (q_s - g_s) R_p^2 A_1 + (u_s - h_s) R_p A_1 + V_s - i_s + P_s e^{r_s R_p A_1}$,
 $x_{33} = r_s \cdot e^{r_s y_d}$, $x_{34} = -r_s \cdot e^{-r_s y_d}$, $x_{35} = -P_s \cdot S_s \cdot e^{r_s y_d} - 2q_s y_d - u_s$,
 $x_{41} = 1 - r_s t_{ox} \frac{\sigma_{Si}}{\sigma_{ox}}$, $x_{42} = 1 + r_s t_{ox} \frac{\sigma_{Si}}{\sigma_{ox}}$,
 $x_{45} = \sqrt{\frac{2}{l}} \frac{1}{r_s} \{(V_G - V_{FB} - V_n)[1 - (-1)^n] + (-1)^n V_D\} - \left(i_s - h_s t_{ox} \frac{\sigma_{Si}}{\sigma_{ox}} \right)$;

$\phi_A(x, y)$ 及 $\phi_B(x, y)$ 中系数的收敛性是令人满意的。验证结果表明, 当 $n=9$ 时, 其值减小为 $n=1$ 时的 10^{-2} 。

由(15)式可得到表面势为:

$$\phi_s(x) = \phi_A(x, 0) = V_n + \frac{V_D}{l} x + \sqrt{\frac{2}{l}} \sum (C_s + D_s + i_s) \sin \cdot r_s x \quad (25)$$

(3) 短沟道 MOS 场效应管阈值电压的解析表达式

短沟道效应主要是由于沟道中沿沟道方向的横向电场的不均匀性引起的^[24]。利用高斯公式可以推得短沟道阈值电压与横向电场梯度的关系。

$$V_T - V_{FB} = 2\phi_F + t_{ox} \frac{\sigma_{Si}}{\sigma_{ox}} \left[\frac{q}{\epsilon_0 \sigma_{Si}} \int_0^{y_d} N(y) dy - \int_0^{y_d} \frac{\partial E_{ss}(x, y)}{\partial x} \cdot dy \right] - V_{TO} - t_{ox} \cdot \frac{\sigma_{Si}}{\sigma_{ox}} \int_0^{y_d} \frac{\partial E_{ss}(x, y)}{\partial x} \cdot dy \quad (26)$$

其中

$$\int_0^{y_d} \frac{\partial E_{ss}(x, y)}{\partial x} dy = \int_0^{R_p A_1} \frac{\partial E_{ss}(x, y)}{\partial x} \cdot dy + \int_{R_p A_1}^{y_d} \frac{\partial E_{ss}(x, y)}{\partial x} \cdot dy \quad (27)$$

$E_{ss}(x, y)$ 为沟道中的横向电场。

在 $0 < y < R_p A_1$ 范围内, 由(15)式。

$$\phi_s(x, y) = V_n + \frac{V_D}{l} x + \sqrt{\frac{2}{l}} \sum (C_s e^{r_s y} + D_s e^{-r_s y} + g_s y^2 + h_s y + i_s) \cdot \sin r_s x$$

$$\begin{aligned}
 E_{xx}(x, y) = & -\frac{\partial \phi_s(x, y)}{\partial x} \\
 = & -\left[\frac{V_D}{l} + \sqrt{\frac{2}{l}} \sum_n r_n (C_n e^{r_n y} + D_n e^{-r_n y} + g_n y^2 + h_n y + i_n) \right. \\
 & \left. \cdot \cos r_n x \right] \quad (28)
 \end{aligned}$$

$$\frac{\partial E_{xx}(x, y)}{\partial x} = \sqrt{\frac{2}{l}} \sum_n r_n^2 (C_n e^{r_n y} + D_n e^{-r_n y} + g_n y^2 + h_n y + i_n) \sin r_n x \quad (29)$$

于是便有

$$\begin{aligned}
 \int_0^{R_{PA1}} \frac{\partial E_{xx}(x, y)}{\partial x} \cdot dy = & \sqrt{\frac{2}{l}} \sum_n r_n^2 \int_0^{R_{PA1}} (C_n e^{r_n y} + D_n e^{-r_n y} + g_n y^2 \\
 & + h_n y + i_n) \sin r_n x \cdot dy \\
 = & \sqrt{\frac{2}{l}} \sum_n r_n^2 \left[\frac{C_n}{r_n} (e^{r_n R_{PA1}} - 1) - \frac{D_n}{r_n} (e^{-r_n R_{PA1}} - 1) \right. \\
 & \left. + \frac{g_n}{3} R_{PA1}^3 + \frac{h_n}{2} R_{PA1}^2 + i_n R_{PA1} \right] \cdot \sin r_n x \quad (30)
 \end{aligned}$$

在 $R_{PA1} < y < y_d$ 范围内, 由(16)式:

$$\begin{aligned}
 \phi_s(x, y) = & V_{ss} + \frac{V_D}{l} x + \sqrt{\frac{2}{l}} \sum_n (\tilde{C}_n e^{r_n y} + \tilde{D}_n e^{-r_n y} + p_n e^{r_n y} + q_n y^2 \\
 & + u_n y + V_n) \cdot \sin r_n x, \\
 E_{xx}(x, y) = & -\frac{\partial \phi_s(x, y)}{\partial x} = -\left[\frac{V_D}{l} + \sqrt{\frac{2}{l}} \sum_n r_n (\tilde{C}_n e^{r_n y} + \tilde{D}_n e^{-r_n y} + p_n e^{r_n y} \right. \\
 & \left. + q_n y^2 + u_n y + V_n) \cdot \cos r_n x \right]. \quad (31)
 \end{aligned}$$

$$\frac{\partial E_{xx}(x, y)}{\partial x} = \sqrt{\frac{2}{l}} \sum_n r_n^2 (\tilde{C}_n e^{r_n y} + \tilde{D}_n e^{-r_n y} + p_n e^{r_n y} + q_n y^2 + u_n y + v_n) \cdot \sin r_n x \quad (32)$$

由此可得

$$\begin{aligned}
 \int_{R_{PA1}}^{y_d} \frac{\partial E_{xx}(x, y)}{\partial x} dy = & \sqrt{\frac{2}{l}} \sum_n r_n^2 \left[\frac{\tilde{C}_n}{r_n} (e^{r_n y_d} - e^{r_n R_{PA1}}) \right. \\
 & - \frac{\tilde{D}_n}{r_n} (e^{-r_n y_d} - e^{-r_n R_{PA1}}) + \frac{p_n}{r_n} (e^{r_n y_d} - e^{r_n R_{PA1}}) \\
 & + \frac{q_n}{3} (y_d^3 - R_{PA1}^3) + \frac{u_n}{2} (y_d^2 - R_{PA1}^2) \\
 & \left. + V_n (y_d - R_{PA1}) \right] \cdot \sin r_n x. \quad (33)
 \end{aligned}$$

四、结果与讨论

在长沟道情况下, 可认为表面势为常数。在短沟道情况下, 表面势是沟道中位置的函数^[1]。本模型计算所得结果与这一结果相符合。图 2 给出在 MOS 管的沟宽 $W = 20\mu\text{m}$, $t_{ox} = 500\text{\AA}$, $V_D = 5\text{V}$, $V_{SG} = 0\text{V}$, 以及砷硼注入能量、剂量分别为 $E_{AS} = 75\text{keV}$, $E_B = 20\text{keV}$, $\phi_{AS} = 5 \times 10^{11}\text{cm}^{-2}$, $\phi_B = 5 \times 10^{10}\text{cm}^{-2}$, 退火温度及时间为 1050°C 及 1800 秒时, 沟长 $l = 0.8\mu\text{m}$, $1.0\mu\text{m}$, $2.0\mu\text{m}$ 的表面势分布图(以下各图不作说明则数据同此)。

图 3 给出由解析公式(26)所算得的 V_T 随沟道长度的变化关系, 其中 t_{ox} 分别为 100\AA , 300\AA , 500\AA , 700\AA 。图 4 给出在 V_D 分别为 1 , 3 , 5V 时阈值电压随沟道长度的变化。显然 V_T 随漏电电压 V_D 的增大而变小。图 5 及图 6 分别给出 V_T 与砷注入能量及硼注入剂量的关系图。由图可见, V_T 随注入能量增加而略有增大, 但变化不大。 V_T 随硼注入剂量的增加而减小, 因此可以通过调节硼注入的剂量来调整阈值电压。图 7 给出阈值电压与退火时间的关系。显然, V_T 随退火时间的增大而减小。由图可见退火时间可较准确地控制 V_T 。图 8 给出阈值电压与退火温度的关系。同样, V_T 随退火温度的提高而减小。图 9 给出解析模型的结果与 MINIMOS 模拟结果的比较, 二者误差小于 5%, 说

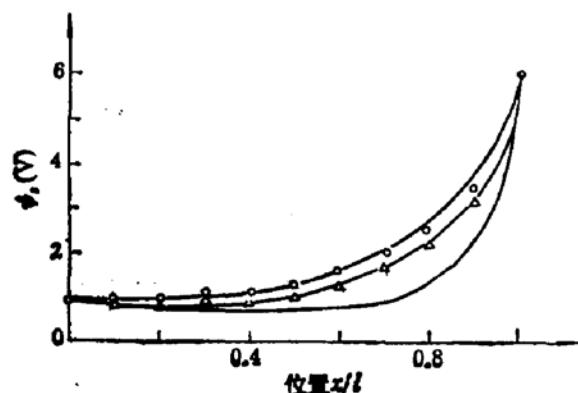


图 2 表面势与 z/l 关系图
 $-\cdots-\circ-\cdots l = 0.8\mu\text{m}$ $-\Delta-\Delta-\Delta-\cdots l = 1.0\mu\text{m}$ $-\cdots l = 2.0\mu\text{m}$

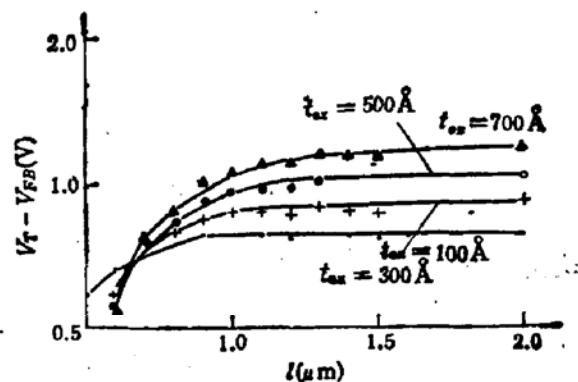


图 3 V_T 与 t_{ox} 关系图

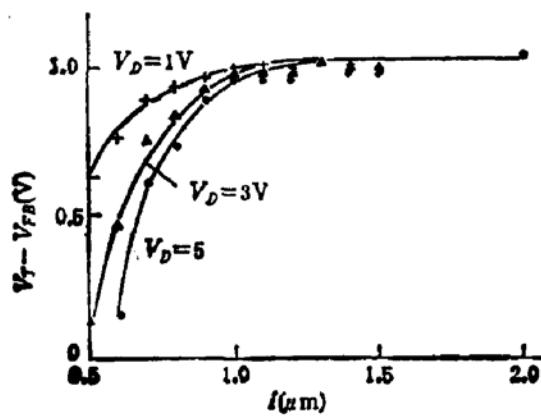


图 4 V_T 与 V_D 关系图

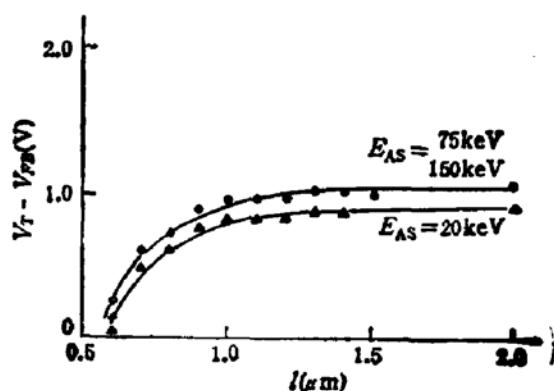


图 5 V_T 与砷注入能量关系图

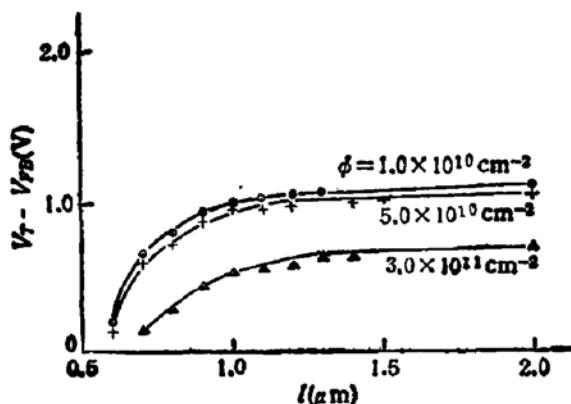
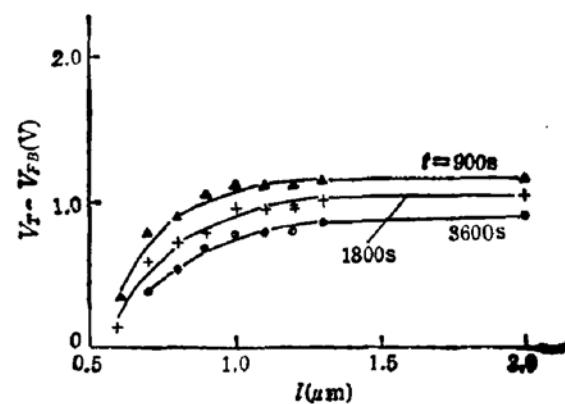
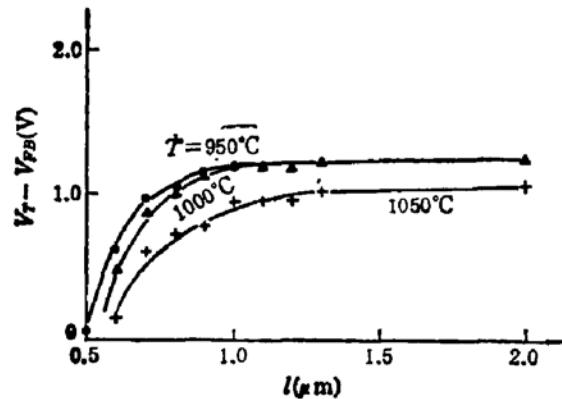
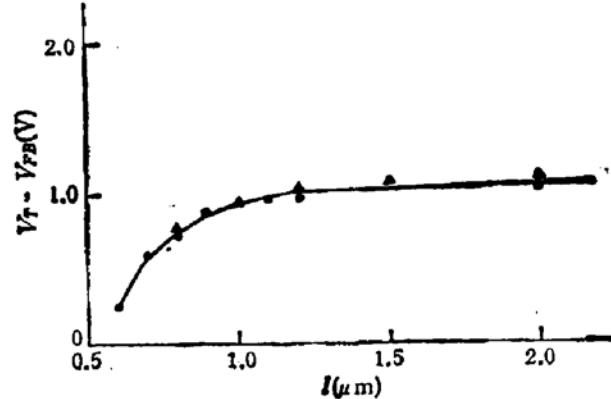
图 6 $V_T - V_{FB}$ (V) 与硼注入剂量关系图图 7 $V_T - V_{FB}$ (V) 与退火时间关系图图 8 $V_T - V_{FB}$ (V) 与退火温度关系图

图 9 解析模型与 MINIMOS 模拟比较图

●●● 解析模型 —▲—▲—▲—MINIMOS 模拟

明本解析模型的结果是比较正确的。

综上所述, 根据解析模型, 离子注入条件及退火条件对器件结构和参数的影响可用下列表格表示:

	Y_I	N_A	y_a	V_{TO}	V_T
A: 剂量↑	↑	↑	↓	↑	↑
B: 剂量↑	↓	↓	↑	↓	↓
A: 能量↑	↑	↓	↑	↑	↑
B: 能量↑	↑	↑	↓	↑	↑
退火时间 (s)	↑	↓	↑	↓	↓
退火温度 (T)	↑	↓	↑	↓	↓

表中 Y_I 为结深, V_{TO} 及 V_T 分别为长沟和短沟 MOS 管阈值电压。

附录

$$\phi(x, y) = V_{DD} + \frac{V_D}{l} x + \sqrt{\frac{2}{l}} \sum A_s(y) \sin \frac{n\pi}{l} x \quad (34)$$

将上式代入二维泊松方程(14)式:

$$\frac{\partial^2 A_s(y)}{\partial y^2} - r_s^2 A_s(y) = \sqrt{\frac{2}{l}} \int_0^l \frac{q}{\sigma_0 \sigma_{s1}} N(y) \sin \frac{n\pi}{l} x \cdot dx = f_s N(y) \quad (35)$$

在 $0 < y < R_{sA0} + 0.5\Delta R_{sA0}$ 范围内,由(10)式可得

$$\frac{\partial^2 A_s(y)}{\partial y^2} - r_s^2 A_s(y) = f_s [(N_{m1}s_1 - N_{mb1})y^2 + (N_{m2}s_1 - N_{mb2})y + (N_{m3}s_0 - N_{mb3}) - N_0] \quad (36)$$

设(36)式的通解和特解分别为

$$\overline{A_s(y)} = C_s e^{r_s y} + D_s e^{-r_s y} \quad (37)$$

$$\overline{A_s(y)} = g_s y^2 + h_s y + i_s \quad (38)$$

将特解代入(36)式,比较两边系数,便可得 g_s 、 h_s 及 i_s 。于是二维电势分布及表面势可分别表示为(15)式及(25)式。

在 $R_{sA0} + 0.5\Delta R_{sA0} < y < y_d$ 范围内,可用同样方法得到系数 ρ_s 、 q_s 、 s_s 及 σ_s ,并得到电势分布(16)式。

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An Analytical Threshold Voltage Model for Short Channel MOS FET With Boron and Arsenic Implantation

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Abstract

The segmental approximation of quadratic function and exponential function are used for describing the distribution of boron and arsenic ion implantation in short channel MOS FET. By using Green's function method, the two-dimensional Poisson's Equation is solved. The analytical model of surface potential and threshold voltage of short channel MOS FET with nonuniform doping profile are derived. The influence of implantation energy, dose and annealing temperature, annealing time on threshold voltage are included in this annalytical model. The influence of drain voltage V_D and thickness of oxidation layer are also included in. The results of the analytical model is in good agreement with the results by using MINIMOS numerical simulation. It is simple and effective and it can be used for improving the model in such circuit analysis programs as in SPICE.

KEY WORDS: Poisson's equation, Ion implantation, Analytical solution, Surface potential, Boundary conditions