

## Self-Aligned InGaP/GaAs Power HBTs with a Low Bias Voltage<sup>\*</sup>

Zheng Liping, Sun Haifeng, Di Haocheng, Fan Yuwei, Wang Suqin, Liu Xinyu and Wu Dexin

(Institute of Microelectronics, The Chinese Academy of Sciences, Beijing 100029, China)

**Abstract:** A self-aligned InGaP/GaAs power HBTs for L-band power amplifier with low bias voltage are described. Base emitter metal self-aligning, air-bridge, and wafer-thinning are used to improve microwave power performance. A power HBT with double size of emitter of  $(3\mu\text{m} \times 15\mu\text{m}) \times 12$  is fabricated. When the packaged HBT operates in class AB at a collector bias of 3V, a maximum 23dBm output power with 45% power added efficiency is achieved at 2GHz. The results show that the InGaP/GaAs power HBTs have great potential in mobile communication systems operating at low bias voltage.

**Key words:** self-aligned; InGaP; power HBTs; low bias voltage

**EEACC:** 2560Z

**CLC number:** TN322<sup>+</sup>.8

**Document code:** A

**Article ID:** 0253-4177(2004)08-0908-05

### 1 Introduction

L-band power amplifiers with single and low bias voltage are greatly required for mobile communication systems. Heterojunction bipolar transistors (HBTs) have strong potential for the application of high-power, high-efficiency microwave solid-state amplifier<sup>[1~3]</sup>. Compared with other solid-state three-terminal devices, HBTs are attractive for power amplifier application for the higher power density operation, higher breakdown voltage, higher impedance values, high efficiency, and operation with single bias supply. Moreover, the optical lithography compatible dimensions of the HBT also make it amenable to high yield, low-cost, volume production.

So far, several researches working on AlGaAs/GaAs power HBTs have very impressive re-

sults<sup>[4~6]</sup>. But due to inherent material limitations, i. e. the two semiconductors (AlGaAs and GaAs) having the same anion (As), AlGaAs/GaAs power HBTs will effectively lower the minority-carrier injection efficiency of the emitter by the existence of conduction band spike. The use of InGaP, instead of AlGaAs, will allow the improvement of minority-carrier injection efficiency and lower  $V_{ce\text{-offset}}$ , a collector emitter offset voltage because of the difference in conduction band discontinuities at the emitter-base and base-collector junctions. In addition, extreme high etching selectivity between InGaP and GaAs will enhance process yield and result in lower base resistance without overetching the base. So, InGaP/GaAs HBTs are preferable to AlGaAs/GaAs HBTs for low-bias voltage and high power operation<sup>[7~9]</sup>.

The research working on the InGaP/GaAs power HBTs in China has never been reported till

<sup>\*</sup> Project supported by State Key Development Program for Basic Research of China(No. 2002CB31190), National Natural Science Foundation of China(No. 60146001), and National Knowledge Innovation Program of CAS.

Zheng Liping female, was born in 1975, PhD candidate. Her research fields are in HBT devices and circuits.

Received 29 December 2003, revised manuscript received 18 March 2004

©2004 The Chinese Institute of Electronics

now. In this paper, we present the design and fabrication of the self-aligned InGaP/GaAs power HBTs operating at low bias voltage at L-band frequency. The device exhibits good microwave power performance.

## 2 Design and Fabrication

The InGaP/GaAs HBTs structures are grown by MOCVD on a semi-insulating GaAs substrate with 4 inch. The thickness of collector has to be chosen by tradeoff between the collector voltage and the transit time delay. A 700nm thick collector is used in the epitaxial structure. The epitaxial structure of the InGaP/GaAs power HBT is shown in Table 1.

Table 1 Epitaxial structure of InGaP/GaAs power HBT

Layer name	Material	Doping /cm <sup>-3</sup>	Thickness /nm
Cap layer	n <sup>+</sup> -In <sub>x</sub> Ga <sub>1-x</sub> As ( $x = 0.6$ )	$> 1 \times 10^{19}$	50
Cap layer	n <sup>+</sup> -In <sub>x</sub> Ga <sub>1-x</sub> As ( $x = 0.6 \sim 0$ )	$> 1 \times 10^{19}$	50
Cap layer	n <sup>+</sup> -GaAs	$5 \times 10^{18}$	120
Emitter layer	In <sub>x</sub> Ga <sub>1-x</sub> P ( $x = 0.5$ )	$3 \times 10^{17}$	50
Base layer	p <sup>+</sup> -GaAs	$4 \times 10^{19}$	60
Collector	n <sup>-</sup> -GaAs	$3 \times 10^{16}$	700
Subcollector	n <sup>+</sup> -GaAs	$5 \times 10^{18}$	500

A self-aligned emitter-base process is used to minimize the base series resistance and base-collector capacitor<sup>[10]</sup>. First, the emitter metal pattern is defined, evaporated, and lift-off. Then, the base is accessed through wet etching, and self-aligned base contacts are deposited on the base layer. Following the base metal evaporation, the collector is accessed through wet etching, and AuGeNi/Ag/Au for collector contact alloys. The collector contact metal is alloyed at 390°C for 1 min. Then, the device is passivated by SiN and SiO. Finally, all emitter contacts are joined together using low parasitic air bridges. The wafer is to be thinned to 100 μm after all the front-side processes are completed. This thickness is chosen as a design compromise between low thermal resistance and low microwave loss. In order to decrease the parasitic effect and die area, we

use the HBT with double emitters. And an emitter-ballasting resistor of 4Ω/finger is included to get the thermal stability. Fig. 1 is the microscope photograph of the device, the emitter size is  $2 \times (3\mu\text{m} \times 15\mu\text{m}) \times 12$ .

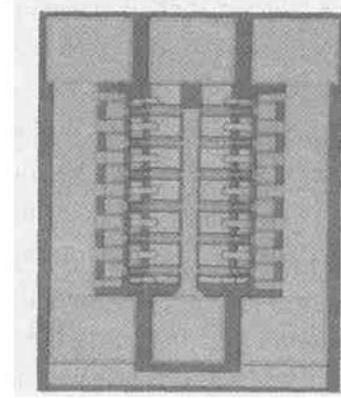


Fig. 1 Microscope photograph of power HBT The emitter size is  $2 \times (3\mu\text{m} \times 15\mu\text{m}) \times 12$ .

## 3 Results and discussion

### 3.1 DC and small signal characteristics

The DC performances of the device are measured by the semiconductor curve tracer. The common emitter  $I$ - $V$  characteristics of the InGaP/GaAs power HBT is shown in Fig. 2, where  $I_b = 1\text{mA/step}$ . Figure 2 shows the DC current gain is about 20 without the current gain collapse that means a 4Ω emitter resistance is enough to avoid current gain collapse. Figure 2 also shows that the  $V_{ce}$ -offset is about 0.3V, the knee voltage is about 0.7V at the current density of  $17\text{kA/cm}^2$ . And the breakdown voltage ( $BV_{ceo}$ ) of the unit InGaP/GaAs HBT is 12V.

The small-signal microwave performances of the power HBT are measured with a HP8510C vector network analyzer and cascade microwave coplanar waveguide probes. Figure 3 shows the measured current gain ( $H_{21}$ ) and maximum available/stable gain ( $G_{max}$ ) as a function of frequency. The  $f_t$  and  $f_{max}$  of the power HBT are 38GHz and 30GHz by extrapolating the current gain and the maximum available/stable gain with a -20dB/oct

roll-off, respectively. 24.5dB, the maximum available gain, was achieved at 2GHz. After package, the small signal power performance of the device at the same bias ( $V_{ce} = 2V$  and  $I_c = 100mA$ ) is measured by Agilent E8363B performance network analyzer. Figure 4 shows the variation of maximum available gain with frequency. The  $f_{max}$  of the same power HBT decreases to 11GHz. 11.5dB, the small-signal maximum available gain ( $G_{max}$ ), was achieved at 2GHz. So, the process of package is crucial to the performance of the power HBT. In order to improve the performance of the packaged power HBT, decreasing the package parasitic parameter in the work frequency and decreasing the emitter series inductance are very important. The Via hole process can decrease the emitter series inductance effectively.

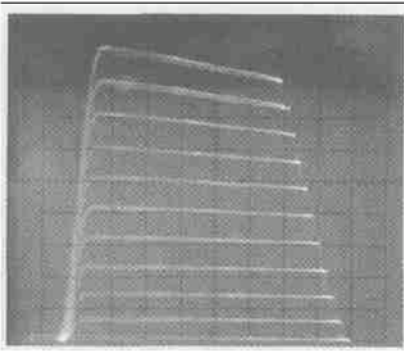


Fig. 2 Common emitter  $I$ - $V$  characteristics of a  $2 \times (3\mu m \times 15\mu m) \times 12$  HBT  $I_b = 1mA/step$ ,  $I_c = 20mA$ ,  $V_{ce} = 0.5V/step$

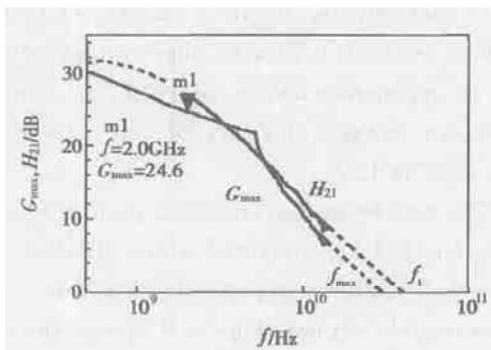


Fig. 3 Measured current gain, maximum available/stable gain of the power HBT as a function of frequency  $V_{ce} = 24V$

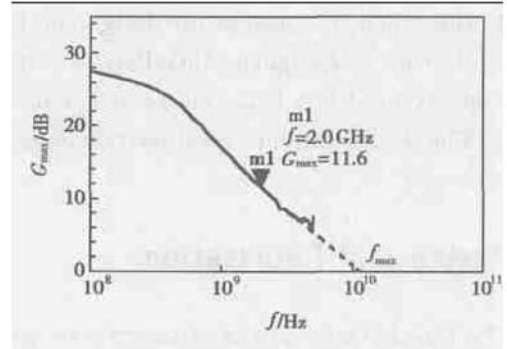


Fig. 4 Measured maximum available gain of the packaged power HBT as a function of frequency  $V_{ce} = 2V$ ,  $I_c = 100mA$

### 3.2 Microwave power characteristics

The CW power characteristics of  $2 \times (3\mu m \times 15\mu m) \times 12$  HBT device at 2GHz are measured with variable sources and load impedance. The packaged power HBT is mounted on Au carriers, and then bonded to microstrip lines on thick alumina substrates mounted on a brass test fixture. The harmonics are not tuned in the matching circuits. Figure 5 shows the measured output power ( $P_{out}$ ), power gain ( $G_p$ ) and power-added efficiency (PAE) at 3V of collector voltage under class AB operation. The load is tuned to a maximum power. When the packaged HBT operates at 3V of collector bias and collector current of 200mA, a 23dBm maximum output power with 45% power added efficiency and 7dB power gain are achieved at 2GHz. The output power at 1dB gain compression ( $P_{1dB}$ ) is 21dBm with 9.5dB of linearity power gain.

Figure 6 is a typical output spectrum acquired from the HP8563E spectrum analyzer, the frequency range is 0.5~ 3.5GHz. The RF input signal frequency is 2GHz. There is an output spectrum at 2GHz. No parasitic clutter is found.

## 4 Conclusion

In this paper, a high performance  $2 \times (3\mu m \times 15\mu m) \times 12$  self-aligned InGaP/GaAs power HBTs with a low bias voltage at L-band frequency is

demonstrated. The measurement results of the device indicate that a maximum 23dBm power output with a linearity power gain of 9.5dB and a 45% maximum power added efficiency with 3V bias un-

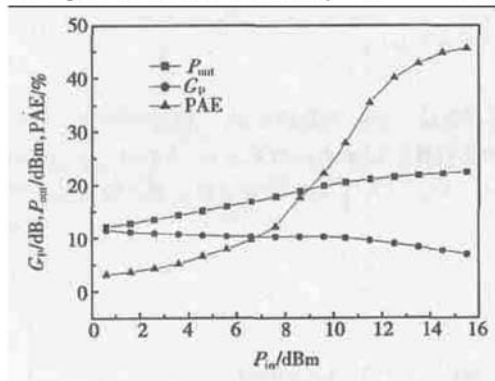


Fig. 5 Measured CW output power, PAE, gain( $G_p$ ) of a  $2 \times (3\mu\text{m} \times 15\mu\text{m}) \times 12$  HBT with  $V_{ce}$  of 3V

der class AB operation are achieved. These results show that InGaP/GaAs power HBTs are suitable for mobile communication systems.

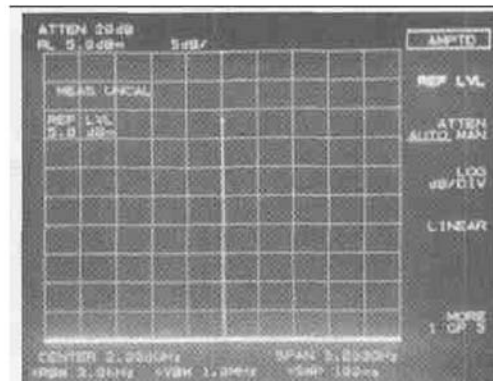


Fig. 6 Output spectrum of the  $2 \times (3\mu\text{m} \times 15\mu\text{m}) \times 12$  HBT with  $V_{ce}$  of 3V

## References

- [1] Liu W. Handbook of heterojunction bipolar transistor. John Wiley&Sons, 1998
- [2] Ali F, Gupta A, Higgins A. Advances in GaAs HBT power amplifiers for cellular phones and military applications. IEEE Microwave and Millimeter-Wave Monolithic Circuits Symposium, 1996: 61
- [3] Wu C S, Pao C K, Hu M, et al. High efficiency X-band power HBT's. IEEE GaAs IC Symposium, 1992: 259
- [4] Hayama N, Kim C W, Takahashi H, et al. High-efficiency, small-chip AlGaAs/GaAs power HBTs for low-voltage digital cellular phones. IEEE MTT-S Digest, 1997: 1307
- [5] Yan B P, Zhang H M, Dai X Y. Self-aligned AlGaAs/GaAs HBT with high power density. Chinese Journal of Semiconductors, 2001, 22(2): 241(in Chinese) [严北平, 张鹤鸣, 戴显英. 高功率密度自对准结构 AlGaAs/GaAs 异质结双极晶体管. 半导体学报, 2001, 22(2): 241]
- [6] Qian F, Chen X J. X-band power heterojunction bipolar transistor. Research & Progress of SEE, 2003, 23(1): 45(in Chinese) [钱锋, 陈效建. X 波段功率异质结双极晶体管. 固体电子学与进展, 2003, 23(1): 45]
- [7] Ueda O, Kawana A. Current status of reliability of InGaP/GaAs HBTs. Solid-State Electron, 1997, 41: 1605
- [8] Fu S T, Yang L W. Low voltage X-band InGaP/GaAs power heterojunction bipolar transistor. IEEE. MTT-S Digest, 1994: 675
- [9] Ohara S, Yamada H, Yamaguchi H, et al. InGaP/GaAs power HBTs with a low bias voltage. IEEE IEDM, 1995: 791
- [10] Zheng L P, Liu X Y, Yuan Z P, et al. Passivation ledge fabrication and its effect on the performance of self-aligned InGaP/GaAs HBT with difference emitter sizes. Chinese Journal of Semiconductors, 2004, 25(3): 312(in Chinese) [郑丽萍, 刘新宇, 袁志鹏, 等. 钝化边的制作及其对不同尺寸自对准 InGaP/GaAs HBT 性能的影响. 半导体学报, 2004, 25(3): 312]

## 低偏置电压工作的自对准 InGaP/GaAs 功率异质结双极晶体管\*

郑丽萍 孙海锋 狄浩成 樊宇伟 王素琴 刘新宇 吴德馨

(中国科学院微电子研究所, 北京 100029)

**摘要:** 介绍 L 波段、低偏置电压下工作的自对准 InGaP/GaAs 功率异质结双极晶体管的研制. 在晶体管制作过程中采用了发射极-基极金属自对准、空气桥以及减薄等工艺改善其功率特性. 功率测试结果显示: 当器件工作在 AB 类, 工作频率为 2GHz, 集电极偏置电压仅为 3V 时, 尺寸为  $2 \times (3\mu\text{m} \times 15\mu\text{m}) \times 12$  的功率管获得了最大输出功率为 23dBm, 最大功率附加效率为 45%, 线性增益为 10dB 的良好性能.

**关键词:** 自对准; InGaP; 功率双异质结晶体管; 低偏置电压

**EEACC:** 2560Z

中图分类号: TN322\*.8

文献标识码: A

文章编号: 0253-4177(2004)08-0908-05

\* 国家重点基础研究发展规划(批准号: 2002CB311902), 国家自然科学基金(批准号: 60146001) 及中国科学院知识创新工程资助项目

郑丽萍 女, 1975 年出生, 博士研究生, 主要从事 HBT 器件和电路的研究.

2003-12-29 收到, 2004-03-18 定稿

©2004 中国电子学会